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Earthquake and Tsunami in Japan on March 11, 2011 and Consequences for Fukushima and other Nuclear Power Plants

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Preliminary Note

- Collection of information about the Tohoku-Taiheiyou-Oki earthquake und tsunami in Japan on March 11, 2011.
- ► Main Idea
 - Provide an impression of the sequence of events.
 - Understand consequences for nuclear power plants.
- All data have principally not yet been verified finally, but have been collected to the best of knowledge.
- The presentation is continuously being updated, as the VGB office gets new information.









Tohoku-Taiheiyou-Oki Earthquake





Source: GRS, 2011 F: Fukushima JST: Japan Standard Time

Northern Honshu Power Supply System





- Northern Honshu is separated electrically (50 Hz) from the southern part (60 Hz).
- Only three frequency converters with a total capacity of ≈ 1 GW.
- Earthquake-induced shutdown of numerous conventional power plants (hydroelectric, fossil-fired) and all nuclear plants (11 units at 4 sites, automatic safety system) in northeastern part of Honshu.
- ► Total Load: ≈ 41 GW
- ► Total Supply: ≈ 31 GW
- Supply Gap: ≈ 10 GW

Tohoku-Taiheiyou-Oki Earthquake





- Vertical Displacement
 D ≈ 7 to 10 m
- Peak Displacement D_{max} ≈ 17 to 25 m⁻¹)
- ► Rupture Zone A ≈ 500 km x 100 km
- Hypo Center Depth Z_H ≈ 20 to 25 km
- ► Crack Velocity v ≈ 2 km/s
- Water Depth Z ≈ 8 km

- ► Rough Estimate of Water Volume Involved V ≈ A · ¼ D ≈ 500 km · 100 km · 2,5 m = 125 km³
- ► Consequence: Sudden displacement of a huge water volume ► Tsunami.

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Topographic Effects



Relative horizontal displacement of Japan, based on GPS data:

≈ 5.2 m (maximum)

- Displacement on rupture surface:
 - ≈ 25 to 27 m
- Rupture length (aftershock):

≈ 400 km

Sea bed lifting:
 up to 7 m



Tohoku-Taiheiyou-Oki Earthquake Intensity





Soolo	Japan	Europe	
Scale	JMA	EMS	
Kurihara	7	11	
Fukushima	6 [↑]	≈ 9 to 10	



- Modified Mercalli Scale (USA)
- Seismic Intensity at Coast: VIII

► There are different scales to estimate local seismic intensities.

Sources: JMA, USGS, 2011 EMS: European Macroseismic Scale JMA: Japan Meteorological Agency USGS: U.S. Geological Service

Tohoku-Taiheiyou-Oki Earthquake Magnitude

- Moment-Magnitude:
- ► Fukushima Design Basis: M_w = 8.2
 - Earthquake effects on the plant depend on the distance between plant and epicenter.
 - At the same location: Moment-Magnitude is by a factor of 10 ^(9.0 − 8.2) ≈ 6.3 higher.

► Richter-Scale for Local Magnitude M_L:

- ► Upper limit on the highest measurable local magnitude (saturation).
- ► All large earthquakes will tend to have a local magnitude of $M_L \approx 7$.
- ► Not applicable (reliable) for earthquakes with large magnitudes.

► Historic Classification: Rank 1 in Japan, Rank 5 Worldwide.

Earthquake	Intensity JMA	Intensity EMS	Magnitude M _w
Tohoku 2011	7	≈ 11	9.0
Basel 1356	≈6↑	9	6.9
Düren 1756	≈6↓	8	5.9
Albstadt 1978	≈ 5 [↑] to 6 _↓	7.5	5.1
Roermond 1992	≈ 5 ↑	7	5.3

 $M_{\rm W} = 9.0$



Chu-Etso Earthquake 2007 Accelerations



► Kashiwasaki-Kariwa Nuclear Power Plant Site

- Located on the inland sea coast of (northwestern) Honshu,
- 5 BWRs (older units) of similar design, based on GE BWR-5,
- 2 ABWRs (newer units) with gas-tight inner and outer containments.

Plant	Seismic Motion	Acceleration in cm/s ²		
		Older Units	Newer Units	
	Design Basis, Plant	167 to 194	254 to 273	
	► Chu-Etso 2007, Plant	384 to 606	332 to 680	
Bedrook	Design Basis, Bedrock	450	450	
Bedrock	► Chu-Etso 2007, Bedrock	1011 to 1478	539 to 1699	

- Chu-Etso earthquake led to accelerations that exceeded the design basis values by a factor of about 2 to 3 without major safety-relevant damages.
- ► In 2011 four of seven units are back in service again after retrofit measures.





	Acceleration ¹) in cm/s ²			
Fukushima	Horizontal		Vertical	
	N-S	E-W		
Daiichi-1	460	447	258	
Daiichi-2	348	550	302	
Daiichi-3	322	507	231	
Daiichi-4	281	319	200	
Daiichi-5	311	548	256	
Daiichi-6	298	444	244	
Design Basis	441	438	412	
Daini-1	254	230	305	
Daini-2	243	196	232	
Daini-3	277	216	208	
Daini-4	210	205	288	
Design Basis	415	415	504	
Shutdown ²)	135 to 150		100	

Measured accelerations were up to 26 % higher than earthquake design basis values for Fukushima Daiichi (≈ 10 % for Onagawa).

Sources: Nied, Wano Tokyo, Tepco, 2011 E-W: East-West N-S: North-South ¹) maximum response, preliminary data ²) threshold for reactor scram



March 11, 2011, 14:46 JST ► Seconds later

- Automatic shutdown (scram) of all operating reactor units within seconds at Onagawa (3), Fukushima Daiichi (3), Fukushima Daiini (4) and Tokai (1).
- Start of the cooling systems to remove residual heat, with an initial value of 6 to 7 % of previous core power and decreasing steadily to less than 0.5 % after some days.
- Turbine room fire at Onagawa-1 (exstinguished hours later).
- Earthquake-induced loss of offsite power at Fukushima-Daiichi.
- Start of some emergency diesel generators as well as relevant cooling systems.
- ► Typical redundancy: 2 + 1 per unit.



Initial Response to Tsunami



About 55 minutes later

- At least Fukushima Daiichi is struck by the tsunami, with a wave height (≈ 14 m) far beyond levee design height (5.7 m) taking out all multiple sets of backup emergency diesel generators (common mode failure).
- Reactor cooling by steam-driven emergency pumps, referred to as reactor core isolation pumps. The relevant auxiliary systems require emergency battery power (8 h).



Tsunami Arrival at Fukushima Daiichi

- Operators follow:
 - abnormal operating procedures,
 - emergency operating procedures, later
 - severe accident management guidelines (SAMGs).

Tsunami Impact at Fukushima Daiichi





Tsunami Impact at Fukushima Daini





2 to 3 m inundation height on the side of unit 1 building.

Tsunami



	Maximum Wave Height ¹)	≈ 23 m	and the second
►	Travel Time from		Fukushima Daiichi
	 Epicenter to Shore 	15 min	
	Epicenter to Fukushima	55 min	
►	Arrival at Fukushima Daiichi	15:41 JST	
►	Wave Height ²)		and the
	at Fukushima Daiichi	≈ 14 m 🗲	Alie I
	at Fukushima Daini	≈ 10 m	
►	Protecting Levee Height		
	Fukushima Daiichi	5.7 m 🔶	
	Fukushima Daini	5.2 m	
►	Ground Level of Reactor Buildings		sale to the second s
	Fukushima Daiichi	≈ 10 m 🗲	
	Fukushima Daini (minimum)	≈7 m	Fukushima Daiichi
	► Onagawa	≈ 20 m	

Practically all damages at Fukushima Daiichi were caused by the tsunami.



Emergency Diesel Generator

Levee Height Design Basis

At Fukushima Daiichi, countermeasures for tsunamis had been established with a design basis height of 5.7 m above the lowest Osaka Bay water level.

≈ 70 m

► As additional safety margin, the ground level had been set to as + 10 m.

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Fukushima Daiichi Aerial View





Fukushima Daiichi Site Layout





Fukushima-Daiichi After Tsunami







- Each unit has an underground trench for piping and cabling that runs from the basement of the turbine building.
- ► These trenches were separately found to be flooded.
- ► Direct results of the tsunami that overwhelmed the power plant.

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Flooded Trenches for Piping and Cabling







Question: Is this accident a matter of residual risk of nuclear energy?

History data of earthquake-induced tsunamis with maximum amplitudes above 10 m
hitting the coasts of Japan and the Kuril Islands (Russia) over the past 513 years

Date and Country		Affected Region	Earthquake ¹)	Tsunami ²)	Victims
11.03.2011	Japan	Japan	M = 9.0	23 m	> 10 000
04.10.1994	Russia	Kuril Islands	M = 8.3	11 m	Not specified
12.07.1993	Japan	Sea of Japan	M = 7.7	31.7 m	330
26.05.1983	Japan	Noshiro	M = 7.7	14.5 m	103
07.12.1944	Japan	Kii Peninsula	M = 8.1	10 m	40
02.03.1933	Japan	Sanriku	M = 8.4	30 m	3 000
01.09.1923	Japan	Tokaido	M = 7.9	12 m	2 144
07.09.1918	Russia	Kuril Islands	M = 8.2	12 m	50
15.06.1896	Japan	Sanriku	M = 7.6	38 m	26 360
24.12.1854	Japan	Nankaido	M = 8.4	28 m	3 000
29.06.1780	Russia	Kuril Islands	M = 7.5	12 m	12
24.04.1771	Japan	Ryukyu Islands	M = 7.4	85 m	13 500
28.10.1707	Japan	Japan	M = 8.4	11 m	30 000
31.12.1703	Japan	Tokaido-Kashima	M = 8.2	10,5 m	5 200
02.12.1611	Japan	Sanriku	M = 8.0	25 m	5 000
20.09.1498	Japan	Nankaido	M = 8.6	17 m	200

Simple Estimation:

Within the past 513 years 16 tsunamis with maximum amplitudes above 10 m and induced by earthquakes of magnitudes between 7.4 and 9.2 have been recorded for Japan and the adjacent Kuril Islands (Russia).

Experienced Frequency:

f = 16/513 a \approx 0.0312 a⁻¹

Thus, within a **thirty** years period one severe tsunami with a maximum amplitude of more than 10 m has to be expected in Japan!

► No, it is rather a matter of obviously having ignored a high specific risk!

Sources: Dr. Johannis Nöggerath, Swiss Nuclear Society, March 28, 2011, www.tsunami-alarm-system.com¹) magnitude²) maximum amplitude

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Is a Japan-like tsunami reasonable for Europe?

- The Atlantic and Mediterranean coasts of Europe are not safe from tsunamis and therefore must be protected.
- In comparison to the Pacific region only a few devasting tsunamis occur in the Atlantic and Mediterranean regions.
- In the Mediterranean on average one devasting tsunami has to be expected every century. About ten percent of all tsunamis taking place worldwide occur in the Mediterranean. Moreover, Greece and Italy are mostly affected by tsunamis in this region.
- Up to now the largest tsunami on the European Atlantic coast took place at Lisbon, Portugal, on November 1, 1755. This tsunami was induced by an earthquake with a magnitude of about 9.0 and had a maximum amplitude of 12 m.

► Conclusion: There is no specific risk for Central Europe.



March 11, 2011, 14:46 JST ► Some hours later at Fukushima-Daiichi

- No restoration of offsite power possible, delays in obtaining and connecting portable diesel generators.
- ► After running out of batteries, loss of heat sink for residual heat.
- Reactor temperatures increase and reactor water levels decrease, eventually uncovering and overheating the reactor cores of units 1 to 3.
- ► Hydrogen production due to oxidation processes in the reactor cores, with main contributions from fuel cladding (Zircaloy) steam reactions at temperatures above ≈ 850 °C (exothermal reaction reinforces the reactor core heatup from radioactive decay power).
- Primary leaks or operator-initiated venting of the reactor cooling systems to relieve the steam pressure (design: 70 bar).
- Release of energy and hydrogen into the inertised primary containment (Drywell) causing primary containment temperatures and pressures to increase (Fukushima Daiichi units 1 to 3).



- Fukushima Daiichi Units 1 to 3: Operator actions to vent the primary containments and to control primary containment pressures and hydrogen levels (required to protect the primary containments from failure).
- Primary containment venting through a filtered (?) path that travels through a duct work in the secondary containment to an elevated release point on the service (refuel) floor on top of the reactor building.
- Hydrogen explosions on service floor of units 1 and 3. Basic requirement: hydrogen concentrations above the lower flammable limit of hydrogen in air (i.e. above 4 volume percent) and activating spark (unit 2 reactor building had eventually been damaged by hydrogen detonation at unit 3).



Unit 1 and Unit 3 Hydrogen Explosions





Mark I Containment General Electric

- Hydrogen explosions in two service floors:
 Unit 1 on March 12,
 - ► Unit 3 on March 14.
 - Concrete reactor building structures remained intact.
 - Reactor building explosion spectacular, but of minor safety importance.

Estimated Hydrogen Production (Recalculation)

- Service floor volume:
- Within flammable range:
- Extent of Core Oxidation:
- ≈ 8000 m³
- ≈ 320 kg H₂
- ≈ 60 to 70 %





Shared spent fuel pool building

Missing heavy oil tanks

Displaced oil tank?

Source: Wano PC, Barrwood, 2011

Unit 3 and Unit 4 after Hydrogen Explosions





Explosion in concrete part of the reactor building of unit 4, although no fuel inside of reactor!

Source: WANO PC, Barnwood, 2011

Units 1 to 4 after Hydrogen Explosions





Aerial View after Hydrogen Explosions









Design of Fukushima Daiichi Unit 1





Design of Fukushima Daiichi Unit 6





Sources: NRC, General Electric

Service Floor of Fukushima Daiichi Unit 1





Service Floor with Primary Containment Head





Source: www.nucleartourist.com

Reactor Pressure Vessel Head






Fuel Assemblies (4)

Plant Design







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Source: Browns Ferry, USA, http://en.wikipedia.org/wiki

Plant Design

Emergency Core Cooling Systems of Different Units at Fukushima Daiichi

- 1) **Residual Heat Removal System**
- 2) Low-Pressure Core Spray (LOCA)
- 3) **High-Pressure Coolant Injection (LOCA)**
- 4) **Reactor Core Isolation Cooling** (Unit 2/3: BWR-4)
- **Isolation Condenser** 5) (Unit 1: BWR-3)
- **Borating System** 6)

Pump Needed





- March 11, 2011, 14:46 JST
 - Earthquake of magnitude 9.
 - The power grid in the northern part of Honshu (Japan) fails.
 - Reactors are mainly undamaged.

Automatic Scram

- Stop of power generation due to fission reaction.
- Further heat generation due to radioactive decay of fission products:







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Containment Isolation

- Closing of all non-safety related penetrations of the containment.
- Turbine hall cut off.
- If containment isolation succeeds, an early large release of fission products is highly unlikely.

Start of Diesel Generators

- Emergency core cooling systems are supplied with electricity.
- Stable Plant State





- ▶ March 11, 2011, 15:41
 - Tsunami hits the plant site.
 - Plant levee design for tsunami wave heights: 5.7 m
 - Actual tsunami height: ≈ 14 m
 - Flooding of diesel generators and/or essential service water buildings.

Station Blackout

- Common cause failure of power supply.
- Only batteries are still available.
- Loss of all emergency core cooling systems, only the pump directly mechanically driven by a steam-turbine is available.





Reactor Core Isolation Pump

- Steam from the reactor core drives a turbine,
- the turbine drives a pump,
- steam condensation in the wetwell,
- water from the wetwell is pumped into the reactor core.
- Requirements:
 - Battery power for steam turbine auxiliaries,
 - the temperature in the wetwell must be lower than 100 °C.
- As there is no heat removal from the reactor building, the work of the reactor core isolation pump is limited.



Reactor Core Isolation Pump Stop

Unit 1: March 11, 16:36, batteries empty,Unit 2: March 14, 13:25, pump failure,Unit 3: March 13, 02:44, batteries empty.

- Decay heat still produces steam in the reactor pressure vessel, leading to a pressure rise.
- Steam discharge into the wetwell due to steam relieve valve opening.
- Decreasing liquid level within the reactor pressure vessel.
- The measured liquid level is the "static" level. The actual swell level is higher due to steam bubbles in the liquid phase.







Core Heatup Phase

- About 50 % of the core cooled by steam only.
- Cladding temperatures rise, but still no significant core damage.
- About 67 % of the core cooled by steam only.
 - Cladding temperatures exceed ≈ 900 °C.
 - Ballooning and/or bursting of claddings (local damages).
 - Release of volatile fission products (noble gases) from internal gaps between fuel pellets and claddings.



Temperature Escalation Phase

- About 75 % of the core cooled by steam only.
 - Cladding temperatures exceed ≈ 1200 °C.
 - Start of significant zirconium oxidation in steam atmosphere.
 Zr + 2 H₂0 ► ZrO₂ + 2 H₂ + Heat
 - Exothermal reaction leads to an additional core heatup.
 - Oxidation of 1 kg of zirconium generates ≈ 44.2 g of hydrogen.
 - Hydrogen production:
 - ▶ ≈ 300 to 600 kg in unit 1,
 - ► ≈ 300 to 1000 kg in units 2 & 3.
- Produced Hydrogen is pushed via the wetwell into the drywell.





TMI-2 Reactor Core Endstate Configuration



- **VGB** PowerTech
- ► Post-accident analyses indicated that ≈ 70 % of core materials had been displaced or damaged.
- Total hydrogen mass produced:

m ≈ 459 kg

This corresponds to a hydrogen volume of about 5500 to 6000 m³ at temperatures between 20 and 50 °C and atmospheric pressure according to the equation of state for an ideal gas:

$$V = \frac{m \cdot R \cdot T}{p \cdot M}$$

with

- m mass M molar mass p pressure R universal gas constant T absolut temperature in K V volume
- Complete oxidation of the zirconium inventory would have led to a hydrogen mass of ≈ 1061 kg.

Core Materials Liquefaction Regimes







Core Melt Progression

- ► At about 1800 °C (Units 1, 2, 3)
 - Melting of metallic cladding remnants and steel structures.
- ► At about 2500 °C (Units 1, 2)
 - Breakdown of fuel rods,
 - inside core debris bed formation.
- At about 2700 °C (Unit 1)
 - Melting of (U, Zr)O₂ eutectics.

Reflood Phase

- Seawater supply stops the core melt progression in the three units.
 - ► Unit 1: March 12, 20:20 ► 27 h without water.
 - ► Unit 2: March 14, 20:33 ► 7 h without water.
 - ► Unit 3: March 13, 09:38 ► 7 h without water.



Release of fission products during core melt progression:

- Xenon, cesium, iodine, ...
- Uranium and plutonium remain in the core.
- Condensation of some fission products to airborne aerosols.

Discharge through valves into the wetwell:

- Pool scrubbing leads to partial aerosol capture in the water.
- Xenon and remaining aerosols enter the drywell:
 - Deposition of aerosols on surfaces leads to further air decontamination.







Containment Safety Function

- Last barrier between fission products and environment.
- Wall thickness: ≈ 3 cm.
- Design pressure: 4 to 5 bar.

Actual Pressures up to 8 bar

- Inert gas filling (nitrogen),
- hydrogen from core oxidation,
- boiling condensation chamber (like a pressure cooker).

Containment Depressurization

- Unit 1: March 12, 04:00,
- Unit 2: March 13, 00:00,
- Unit 3: March 13, 08:41.





Containment Depressurization

- Positive and negative aspects:
 - Removes energy from the containment (only way left),
 - reduces pressure to ≈ 4 bar,
 - release of
 - Small amounts of aerosols (iodine, cesium ≈ 0.1 %),
 - ► all noble gases,
 - ► hydrogen.
- The gas mixture is released onto the reactor service floor.





► Units 1 and 3:

- No recombiners (?).
- Hydrogen explosion inside the reactor service floor.
- This leads to destruction of the steel-frame construction.
- Reinforced concrete reactor building remains undamaged.







► Unit 2:

- Probable damage of drywell following a pressure increase within the reactor pressure vessel and containment.
- Highly contaminated water.
- Uncontrolled release of gas from the containment.
- Release of fission products.
- Temporary plant evacuation due to high local dose rates on the plant site.





► Reactor Status as of March 24:

- Core damage in units 1, 2, 3.
- Damaged reactor buildings of units 1 to 4.
- Reactor pressure vessels of all units are fed with seawater or sweet water by mobile pumps.
- Estimates of General Electric indicate that about 45 tonnes of salt could have been injected into the reactor cores so far, with possible impacts on the reactor core coolability.





• Changes as of March 29:

- External power supply has been recovered for all reactors.
- Control rooms of units 1 and 3 have lighting, technicians test the functionality of the existing emergency feedwater pumps and will replace damaged pumps in the short term.
- Fresh water is supplied from some nearby hydro-reservoirs (tanks?), thus banning dangers of reduced cooling by salt crusts on the fuel rod surfaces and of reduced heat transfer in fuel ponds due to salt after sea water intrusion.





Central control room after lighting has been restored on March 25, 2011.



Source: AREVA NP, March 24, 2011

Spent Fuel Transfer Pools

Spent Fuel Stored in Pool on the Reactor Service Floor:

- The entire core of unit 4 had been stored in the spent fuel pool for maintenance reasons before the earthquake.
- Dry-out of spent fuel pools:
 - unit 4 in ten days,
 - other units in a few weeks.
- Leakage of the spent fuel pools due to earthquake?

Consequences:

- Fuel melting "on fresh air",
- nearly no retention of fission products within the plant,
- possible large release.





Spent Fuel Transfer Pools & Shared Pool



Unit	Number of Assemblies	Water m ³	Power MW	Fresh Core	Cooling	Fuel Damage
1	292	1020	0.3	No	?	?
2	587	1425	1.0	No	Steam Plume	?
3	514	1425	0.7	No	Boiling	?
4	1331	1425	3.0	Yes	Pump Car	Major
5	946	1425	4.5	Probably	Diesel ²)	No
6	876	1497	1.5	Probably	Diesel	No
S	6291 ¹)	?	?	No	Working	No

Fukushima-Daiichi

- ► Unit 1: 400 fuel rod assemblies,
 - 548 fuel rod assemblies.
- Units 2 to 5:
 Unit 6:
 - 764 fuel rod assemblies.
- Unit 3: Small number (32) of ten years old old mixed oxide (MOX) fuel assemblies in spent fuel pool. No significant difference of plutonium inventory compared to other pools, since uranium fuel also contains plutonium, but old MOX fuel contains higher amounts of Americium (more volatile than plutonium).

Unit 4 Spent Fuel Transfer Pool Cooling



150 tonnes of sea water were poured into the spent fuel pool of unit 4 using a concrete pump car on March 22. This action took about three hours and was repeated over hours later.





The concrete pump has a maximum capacity of 120 t/h, is equipped with an **arm** of 58 m maximum length and operated by **12 persons** (remotely).

Unit 4 Spent Fuel Transfer Pool Cooling





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Source: www.cryptome.org, 2011

Unit 4 Spent Fuel Transfer Pool Cooling





April 4, 2011:

Four additional concrete pumps (62 m, 70m) are underway by Antonov airlift from Germany and USA.

Fukushima Daiichi Refueling Cooling System

Dose Rates at Fukushima Daiichi

Date and Local Time (JST) of Measurement

Source: GRS, March 30, 2011 JST: Japan Standard Time

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Dose Rates at Fukushima Daini

Source: GRS, March 30, 2011 JST: Japan Standard Time

From Start of Emergency Procedures

- **Evacuations** according to risk within a 20 km radius.
- Core cooling recovery as far as possible by flooding of reactor cores based on
 - mobile diesel pumps and/or
 - recovery of external power supply,
 - ▶ successful for units 1 and 2 on March 20,
 - ▶ units 3 and 4 following.
- Spent fuel pool cooling recovery by helicopters and/or water cannons for unit 4.
 - Mobile diesel pumps and concrete pump cars for other units (?) and/or
 - recovery of external power supply,
 - ▶ successful for unit 1 on March 20,
 - ▶ units 2 to 4 following.

Fukushima Daiichi, Status as of March 19, 2011 VGB

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U	1	2	3	4	5	6
Core and fuel integrity	Damaged	Damaged	Damaged	No fuel in the reactor	Not Damaged	Not Damaged
Reactor Pressure Vessel Integrity	Unknown	Unknown	Unknown			
Containment Integrity	Not Damaged	Damage Suspected	Might be not damaged	Not Damaged	Not Damaged	Not Damaged
Reactor building integrity	Severely Damaged	Slightly Damaged	Severely Damaged	Severely Damaged	Open a vent hole on the rooftop for avoiding hydrogen explosion	Open a vent hole on the rooftop for avoiding hydrogen explosion
Water injection to core	Continuing (Seawater)	Continuing (Seawater)	Continuing (Seawater)	Not necessary	Not necessary	Not necessary
Water injection to Containment Vessel	Continuing (Seawater)	to be decided (Seawater)	Continuing (Seawater)	Not necessary	Not necessary	Not necessary
Fuel integrity in the spent fuel pool	Water injection to be considered	no info	level low - water injection	level low - preparing water injection	Pool temperature increasing	Pool temperature increasing

Fukushima Daiichi, Status as of April 2, 2011

Unit	1	2	3	4	5	6	
Reactor Type	BWR-3	BWR-4	BWR-4	BWR-4	BWR-4	BWR-G	
Thermal Power	1380 MW _{th}	2381 MW _{th}	2381 MW _{th}	2381 MW _{th} 2381 MW _{th}		3293 MW _{th}	
Electric Power	460 MW _e	784 MW _e	/ _e 784 MW _e 784 MW _e		784 MW _e	1100 MW _e	
Status before earthquake	In service ► auto shutdown	In service ► auto shutdown	In service ► auto shutdown	Outage	Outage	Outage	
Core and fuel integrity	Damaged	Severe Damage	Damaged	No fuel in reactor			
Reactor outside temperatures	250 °C 128 °C	180 °C 450 °C	90 °C (?) 150 °C	Not applicable due to			
Containment integrity	Pressure of 2 bar, flooded?	Pressure of 1 bar, damage suspected	Pressure of 1 bar, damage suspected	outage plant status	Cold Shutdown		
AC Power	Yes plus control room light	Yes plus control room light	Yes plus control room light	Yes plus control room light	existing plar and offsite el-	ntained by it equipment ectrical power	
Building	Severe damage	Slight damage	Severe damage	Severe damage			
Reactor water level	40 % of fuel uncovered	30 % of fuel uncovered	50 % of fuel uncovered	Not applicable due to			
Reactor pressure	About 5 bar, decreasing	Less than 1 bar (?)	1 bar	outage plant status			
Status of spent fuel pool	Fresh water by concrete pump car	58 °C, sea water and fresh water by pool cooling	Sea water and fresh water by concrete pump car	Sea water and fresh water by concrete pump car	32 ° C, pump repaired	24 °C	

Fukushima Daiichi

Unit	INES-Level			
1	7			
2	7			
3	7			
4	3			
5	not specified			
6	not specified			

Fukushima Daini

Unit	INES-Level
1	3
2	3
3	not specified
4	3

Radiology

Lethal Dose ¹): 5000 mSv

Plant	Status	Diesels, pumps	Venting	Offsite power	Damages
Fukushima Daini Units 1 to 4	cold shutdown	?	prepared	available	tsunami?
Onagawa Units 1 to 3	cold shutdown	at least one, one pump	no	available	fire in unit 1, extinguished, no tsunami damage due to the higher ground level
Tokai Unit 2	cold shutdown	one of three, one emergency pump	no	?	safe status
Rokkasho Reprocessing	none	available	not required	?	not reported
Open Questions



- ► Reasons for explosion in reactor building of Fukushima Daiichi unit 4?
- Status of melted reactor cores?
- Status of pool inventories?
- Details of release history?
- ► Venting in Fukushima Daini?
- Draining of trenches?
- Reasons for obviously having ignored the tsunami data base?
- Recriticality in Fukushima Daiichi unit 2?
 (according to soil samples > might explain radioactivity spike on March 16, 2011)



► Tentative by April 4, 2011

- 4 persons dead (2, earthquake, stack cabin in Fukushima Daiini),
- 2 persons missing (found on April 3 as having been drowned),
- **20+ persons injured** (mostly by Hydrogen exlosions),
- less than 20 persons exposed to radiation doses < 250 mSv, (including 3 workers who tried to lay cables in the flooded unit 2 basement on April 1).
- 0 persons exposed to radiation doses > 250 mSv (i.e. one additional late cancer case out of 100 persons).



Design basis for nuclear power plants in Japan:

- ► Incident rate of one earthquake within a **50 000 years** period.
- Incident rate of one large ¹) tsunami within a 30 years period.

Design basis for nuclear power plants in Germany:

Incident rate of one earthquake within a 100 000 years period in combination with relevant flood water heights to be presumed.



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